



# **Cross-laminated timber**

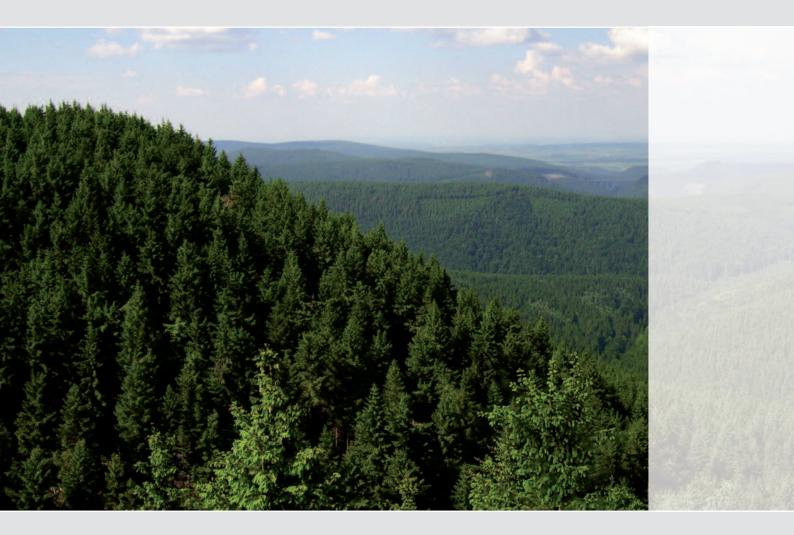
Large-format construction components for roofs, ceilings and walls XXL





# **Building with cross-laminated timber**

Efficient construction with large load-bearing construction components for roofs, ceilings and walls



X-LAM is cross-laminated timber that combines the best properties of different materials as load-bearing plate or panel construction components. X-LAM is a solid material with a considerable load-bearing capacity. These prefabricated components are easy and fast to install on site - equally well for roofing, ceilings or walls. Cross-laminated timber consists of three or more layers of sawn timber glued together at right-angles. The innovative building material replaces brickwork and concrete, and filigree wideslabs, and complements timber-frame construction components.





As manufacturer and supplier of laminated products, we serve the whole spectrum of laminated timber construction.

We see ourselves primarily as partners for architects, timber-construction companies and building contractors.

## Our services:

- ConsultingPlanning
- CNC processing
   Supply
- Structural calculation
- Production
- culation Assembly support services (if required)









# Roof, ceiling, wall - all with one material



# At a glance

### BOARD DIMENSIONS:

Length: 6.00 to 17.80 m Width: up to 3.50 m Thickness: up to 400 mm

### TIMBER SPECIES / STRENGTH CLASSES:

Spruce C24 Moisture content 10%  $\pm$  2% Moulded density: approx. 450 kg/m<sup>3</sup> (other timber species and strength classes on request)

### GLUEING - ADHESIVE BASED ON MELAMINE RESIN:

Adhesive type 1 to EN 301, approved for glueing load-bearing timber components for interiors and exteriors, weather-resistant with transparent glue line (emission class E1)

**CUTTING AND PROCESSING:** with 5-axis CNC portal machine, to customer specifications

### COMPUTED BURN RATE:

0.65 mm/minute

# Clear benefits...

### ... for planners

- European Technical Approval
- Individual design options
- Not limited to standard dimensions
- Large size
- High load-bearing capacity
- High level of fire protection
- Earthquake-resistant

### ... for building contractors

- Pleasant room atmosphere
- Economical construction method
- High degree of prefabrication
- Short times for building and fitting
- Solid construction components
- Heat protection in summer
- Dimensionally stable

### ... and for the environment

- CO<sub>2</sub>-neutral
- Excellent ecobalance
- Airtight and windproof
- PEFC certified
- FSC<sup>®</sup> certified

Construction components made of cross-laminated timber are cut to size and are not constrained to have standard dimensions. This gives freedom for individual design. The data needed for planning is given in the European Technical Approval (ETA) and can be applied to projects rapidly with our draft design program. Buildings made with cross-laminated timber are advantageous, including in earthquake zones, because of their low mass and high strength.

The natural building material wood is the preferred choice when there are high demands on a pleasant and comfortable atmosphere in the rooms. The high level of prefabrication results in fast building and assembly times, which makes the solid construction components very economical. Low thermal conductivity and high thermal protection in summer ensure comfortable living and save energy.

The raw material for making cross-laminated timber is currently exclusively softwood. As a business certified by FSC<sup>®</sup> and PEFC, we focus on sustainable, careful and responsible forestry. Compared to other solid construction methods, the manufacture and processing of cross-laminated timber components requires only little energy and contributes to long-term CO<sub>2</sub> storage and so to minimising the greenhouse effect.

### CHANGE OF SHAPE:

Il to the panel 0.01 % per % of timber moisture change  $\perp$  to the panel 0.20 % per % of timber moisture change

Thermal conductivity $\lambda$ :	0.13 W / (mK)
Specific heat capacity c:	1.61 kJ / (kgK)
Water vapour diffusion resistance $\mu$ :	20-50

### APPROVALS:

ETA-11/0189 EEC conformity declaration PEFC certificate (production sites Niederkrüchten and Westerkappeln) FSC<sup>®</sup> certificate (production sites Niederkrüchten and Westerkappeln)



# Nature meets high-tech - cross-laminated timber in use



### Feel-good rooms from moisture equilibrium

Timber can take up and release moisture - depending on the surrounding atmosphere. This property results in a very comfortable atmosphere in the room. It is natural that a change in moisture also brings a change in volume - swelling and shrinkage.

This is where the high-tech material, cross-laminated timber, scores because this effect can be ignored in planning for normal applications. The transverse glueing of the boards together with the kiln drying of the lamellae to a timber moisture of  $10 \pm 2\%$  minimises the change of volume. This value corresponds to the expected equilibrium moisture content during later use of the building.

This equilibrium property has an effect on the appearance of the surface. Mainly the outer layers of the crosslaminated timber take up moisture during transport and the building phase, depending on the weather situation.

### Careful equalization of the moisture preserves the appearance

The moisture content during construction must be adjusted gradually to the equilibrium moisture content of the later use by careful heating and ventilation. If the indoor climate becomes too dry because the room has been warmed up too fast, the surface of the X-LAM panels will release too much moisture, so that this effect cannot be compensated. Shrinkage cracks and gaps can then occur on the surface of the X-LAM components, especially in the area of the joints of the lamellae. To avoid uncontrolled stress cracks, the edges of the lamellae are not glued.

### Timber is a natural and non-homogeneous construction material

Surface qualities can be precisely and reproducibly defined only to a limited extent. In cases of doubt, the surface quality should be inspected at the factory or in reference projects and agreed between the planner, manufacturer and builder.

Load-bearing components made of X-LAM are constructional components designed for structural use and carefully manufactured from an improved material. Subsequent apertures, notches, additional loads and other changes of the static system must always be agreed with the responsible structural engineer.

### Treatment of visible surfaces

The requirements for the later surface quality must be determined at the planning phase. Construction components of X-LAM have the advantage that they can be the finished surface at the same time. In contrast to buildings where the surfaces are formed afterwards, a high level of quality in the shell construction phase is decisive for a perfect end result.

For visible surfaces we recommend:

- protection of the components from damage and dirt during transport and construction;
- minimising the uptake of water as far as possible (condensation-free covering, avoid entry of rain);
- rapid roofing and closing of the building;
- targeted agreement and guidance of the subsequent trades during the construction phase and demonstration of the material-specific properties;
- avoiding large changes in the room atmosphere;
- arranging the use of the building for standard atmospheres (i.e. 40% to 60% air humidity);
- allow for or obtain tenders for any required cosmetic reworking on the visible surfaces;
- coating the components with our BSH varnish as additional protection from moisture uptake and dirt during transport and assembly.



Rapid roofing will provide the best protection of visible surfaces from weathering effects.

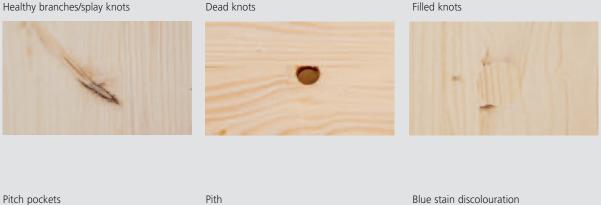
Even with very careful manufacture and only small variations of moisture content, cracks and/or gaps between the lamellae cannot be entirely prevented because of the nature of the material. Coatings, particularly in bright colours, make the cracks and gaps more visible. We explicitly advise against allowing cost considerations to result in visible industrial quality instead of living-space quality.

For static construction components the outer layer thickness has an entirely beneficial effect on the load-bearing performance of the component. On the other hand, thicker lamellae tend to greater swelling and shrinkage, resulting in increased formation of cracks and/or gaps. A good compromise between structural and visual demands is to have lamellae up to 30 mm thick.

## Appearance as required Surface quality

Wall and ceiling components of cross-laminated timer can be produced in various surface qualities depending on requirements. We distinguish non-visible quality (NSI), visible industrial quality (ISI) and living-space quality (WSI). The choice of surface quality depends on the subsequent use of the panel and should be considered at an early planning stage.

X-LAM is a natural product that, unlike synthetically manufactured materials, cannot always be manufactured with the exactly identical appearance. The qualitative characteristics therefore vary within a single surface quality. Various criteria can be used to assess surfaces:







Blue stain discolouration



### Joint width



### Glue penetration



### Traces of planing



### Non-visible quality (NSI)

The material is not visible because the load-bearing walls and ceilings are subsequently covered on-site. In accordance with the requirements of European approval the selection of the initial lamellae is, purely for structural reasons, from strength class C24 and with a small proportion of strength class C16.

- Between the lamellae, gaps up to 6 mm are permitted in the transverse layers and up to 3 mm in the longitudinal layers.
- Discolourations such as blue stain, and red and brown scratch-resistant stripes are permitted.
- Dead knots, even a large number, are not repaired.
- Depending on the glueing technology, adhesive can leak at the surface of the panels.





NSI quality with many marks

NSI quality with few marks

### Visible industrial quality (ISI)

Use of visible industrial quality is to be recommended when the client wishes to see the wood structure and accepts the naturalness of the product. This surface quality is usually adequate for the requirements of office, industrial and commercial buildings but implies a certain tolerance regarding the quality level.

- For the exterior specially sorted and finger-jointed lamellae are used.
- Healthy tightly intergrown knots and splay knots, and sporadic black knots are permissible.
- Dead knots  $\geq$  30 mm are repaired with knot hole plugs, etc.
- There is practically no fungus, insect infestation or blue stain discolouration.
- Pitch pockets and visible pith are permissible.
- Based on the production moisture content of  $10 \pm 2\%$ , the maximum joint width between two lamellae is limited to 4 mm.
- In isolated cases, glue penetration between the lamellae can occur.
- After manufacture, the industrial-quality surface is sanded again. There can still be some visible traces of planing.





ISI quality with few marks

ISI quality with many marks

# **Surface quality**



### Standard structure living-space quality (WSI)

This quality standard meets the requirements for visible surfaces in residential construction. Normally only one side of the panel is produced as a visible surface. The surface quality is achieved by glueing on a laminated solid timber panel that meets the particular criteria of this quality level. It is load-bearing and replaces the outer layer of the cross-laminated timber panel.

- The surface of the solid timber panels meets the criteria of AB sorting as in table 1 of EN 13017-1.
- The panels are as a rule butt-joined without gap, but with production moisture of  $10 \pm 2\%$  a maximum joint width of 2 mm is tolerable.



Standard product, WSI quality: A laminated solid timber panel replaces the exterior surface of the X-LAM component.

The design of the panels for appearance differs for panels with vertical loading (walls) and panels with horizontal loading (roof and ceiling structures). For walls, the outer layers are usually transverse to the longitudinal axis of the panel, or perpendicular when installed. For horizontally loaded panels, the outer layers run parallel to the longitudinal axis of the panel.

### **Special structures**

Alternatively, the X-LAM panels can also be covered with other materials. For example, three-layer boards or OSB panels are suitable. This structure is not load-bearing and must be applied to the panel construction as an additional layer.



CLT element with glued-on three-layer board

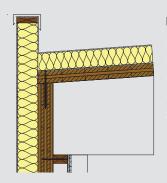


CLT element with glued-on OSB panel

# Example structures Industry and commerce

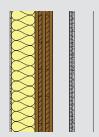
# Benefits of laminated timber construction in industrial buildings:

- The interior surfaces of the walls and ceilings can remain visible. Installations are arranged as wall-mounted installations. Alternatively, low-cost cladding with plasterboard or gypsum fibreboard can be done.
- Building the roof and walls with diaphragm action makes fixed concrete supports unnecessary.
- Economical walls using large-format panel construction
- Easy connections
- Rapid assembly
- Later modifications and extensions are usually possible without great expenditure.



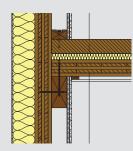
### Roof structure

- Two-layer welded sheet
- Resilient insulation 120 mm
- Vapour barrier / wind seal
- X-LAM L-80/3s
- U value 0.26 W/m $^{2}$ K



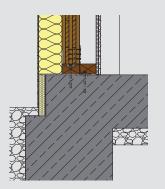
### Wall structure

- Mineral plaster
- Insulation mineral fibre 140 mm
- X-LAM X-100/5s
- Service cavity
  - Gypsum fibreboard
  - U value 0.24 W/m<sup>2</sup>K



### **Ceiling structure**

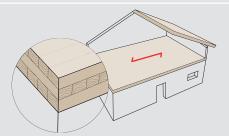
- Screed
  - Impact sound insulation
  - X-LAM L-110/5s
  - Battens (substructure)
  - Gypsum plasterboard



### Floor plate wall joint

Without concrete upstand
 With guide threshold

# Superstructures with maximum flexibility



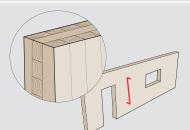
### Ceiling and roof structures

The structure of **L panels** is designed for use in ceiling and roof structures where the main loading is flexure. The outer layers are therefore oriented longitudinally to the panels.

Designation <sup>1)</sup> [-]	Nominal thickness [mm]	s Lamellar structure <sup>2)</sup> [mm]	Dead load <sup>3)</sup> [kN/m²]	Layers	
L-60/3s	60	1201 20 1201	0.27	3	
L-80/3s	80	I30I 20 I30I	0.36	3	
L-90/3s	90	I30I <u>30</u> I30I	0.41	3	
L-100/3s	100	1401 <u>20</u> 1401	0.45	3	
L-110/3s	110	1401 <u>30</u> 1401	0.50	3	
L-120/3s	120	1401 <u>40</u> 1401	0.54	3	
L-130/5s	130	1301 <u>20</u> 1301 <u>20</u> 1301	0.59	5	
L-140/5s	140	1401 <u>20</u> 1201 <u>20</u> 1401	0.63	5	
L-150/5s	150	1301 <u>30</u> 1301 <u>30</u> 1301	0.68	5	
L-160/5s	160	1401 <u>20</u> 1401 <u>20</u> 1401	0.72	5	
L-170/5s	170	1401 <u>30</u> 1301 <u>30</u> 1401	0.77	5	
L-180/5s	180	1401 <u>30</u> 1401 <u>30</u> 1401	0.81	5	
L-200/5s	200	1401 <u>40</u> 1401 <u>40</u> 1401	0.90	5	
L-220/7s	220	1401 <u>20</u> 1401 <u>20</u> 1401 <u>20</u> 1401	0.99	7	
L-240/7s	240	1401 <u>20</u> 1401 <u>40</u> 1401 <u>20</u> 1401	1.08	7	
L-260/7s	260	1401 <u>30</u> 1401 <u>40</u> 1401 <u>30</u> 1401	1.17	7	
L-280/7s	280	1401 <u>40</u> 1401 <u>40</u> 1401 <u>40</u> 1401	1.26	7	
L-290/9s	290	40  <u>30</u>  30  <u>30</u>  30  <u>30</u>  30  <u>30</u>  40	1.31	9	
L-310/9s	310	1401 30 1401 30 1301 30 1401 30 1401	1.40	9	
L-320/9s	320	1401 30 1401 30 1401 30 1401 30 1401	1.44	9	
L-360/9s	360	1401 40 1401 40 1401 40 1401 40 1401 1401	1.62	9	
LL-190/7s	190	1301 1301 <u>20</u> 1301 <u>20</u> 1301 1301	0.86	7	
LL-210/7s	210	1301 1301 <u>30</u> 1301 <u>30</u> 1301 1301	0.95	7	
LL-230/7s	230	1301 1301 <u>40</u> 1301 <u>40</u> 1301 1301	1.04	7	
LL-240/7s	240	1401 1401 <u>20</u> 1401 <u>20</u> 1401 1401	1.08	7	
LL-260/7s	260	1401 1401 <u>30</u> 1401 <u>30</u> 1401 1401	1.17	7	
LL-280/7s	280	1401 1401 <u>40</u> 1401 <u>40</u> 1401 1401	1.26	7	
LL-300/9s	300	1401 1401 20 1401 20 1401 20 1401 1401	1.35	9	
LL-330/9s	330	1401 1401 <u>30</u> 1401 <u>30</u> 1401 <u>30</u> 1401 1401	1.49	9	
LL-360/9s	360	1401 1401 40 40 40 40 40 40 40 40 40 40 40	1.62	9	
LL-400/11s	400	1401 1401 30 1401 30 1401 30 1401 30 1401 140	)  1.80	11	

Table 1

The crosswise structure makes X-LAM components very dimensionally stable and able to take loads along, and transverse to, the main loading direction. In addition to our depicted standard structure designs, we also produce variant structures on request.



### Wall structures

The structure of **X panels** is optimised for use in constructing walls that are mainly loaded by vertical forces in the plane of the panel. The outer layers are therefore oriented transverse to the panel longitudinal direction.

<b>Designation</b> <sup>1)</sup> [-] [mm]	Nominal thickness [mm]	Lamellar structure <sup>2)</sup> [kN/m <sup>2</sup> ]	Dead load <sup>3)</sup>	Layers	
X-60/3s	60	<u>20</u>  20  <u>20</u>	0.27	3	
X-70/3s	70	<u>20</u> I30I <u>20</u>	0.32	3	
X-80/3s	80	<u>30</u> 1201 <u>30</u>	0.36	3	
X-90/3s	90	<u>30</u> 1301 <u>30</u>	0.41	3	
X-100/3s	100	<u>30</u> 1401 <u>30</u>	0.45	3	
X-110/3s	110	<u>40</u> I30I <u>40</u>	0.50	3	
X-120/3s	120	<u>40</u>  40  <u>40</u>	0.54	3	
X-100/5s	100	<u>20</u>  20  <u>20</u>  20  <u>20</u>	0.45	5	
X-110/5s	110	<u>20</u> 1201 <u>30</u> 1201 <u>20</u>	0.50	5	
X-120/5s	120	20  30  20  30  20	0.54	5	
X-130/5s	130	<u>30</u> 1201 <u>30</u> 1201 <u>30</u>	0.59	5	
X-140/5s	140	40 1201 20 1201 40	0.63	5	
X-150/5s	150	<u>30</u>  30  <u>30</u>  30  <u>30</u>	0.68	5	
X-160/5s	160	<u>40</u> 1201 <u>40</u> 1201 <u>40</u>	0.72	5	
X-170/5s	170	40  30  <u>30</u>  30  <u>40</u>	0.77	5	
X-180/5s	180	40 I30I 40 I30I 40	0.81	5	
X-190/5s	190	<u>40</u>  40  <u>30</u>  40  <u>40</u>	0.86	5	
X-200/5s	200	$\overline{\underline{40}}$  40  $\overline{\underline{40}}$  40  $\overline{\underline{40}}$	0.90	5	

<sup>1)</sup> Unless further specified, the design of the outer layers is in non-visible quality. <sup>2)</sup> Marking of the lamellar structure: X= 120I = Orientation of lamellae of the layer in the panel longitudinal direction; L=  $\overline{20}$  = Orientation of lamellae of the layer in the panel transverse direction <sup>3)</sup> The element weight was determined with a molded density of  $\rho$  = 450 kg/m<sup>3</sup>.



Table 2

# Fasteners

### Joining cross-laminated timber elements together (general)

In principle all the usual fasteners used in timber construction can be used, such as dowel pins, fit bolts, nails (with sheet metal parts), clamps (for fishplates) and screws. Full-thread screws are preferable, characterised by high load-bearing capacity and fast assembly (no pre-drilling).

### Anchoring wall elements to the floor plate

We use various angle connectors fixed in the X-LAM element with annular ring nails (or screws) and in the concrete by heavy-duty anchors.

Suitable anchor bolts are fischer FAZ II; depending on the condition of the concrete, concrete bolts or chemical anchors may also be used.



Full-thread screw from SPAX ® Picture: © SPAX International GmbH & Co. KG



fischer FAZ II anchor bolt for fixing angle connectors Picture: © fischerwerke GmbH & Co. KG

### Attachment devices

Erection loops are a simple and economical means of correctly loading the panels. The loops are attached to the wood using a screwed-on wooden block.

For transporting X-LAM panels combi-head wood screws can alternatively be screwed into the plane sides (ceiling or roof elements) or narrow sides (wall elements). For load-bearing devices, universal head connectors are used that enclose the bolt head and can be rotated in all directions for attaching to a crane.

Another alternative are blind holes for taking a short lifting strap that transfers the force to a horizontally arranged dowel pin.

Fasteners, anchors and attachment devices are available from various notable manufacturers.

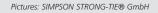








Simpson Strong-Tie ® Angle connector ABR90





Simpson Strong-Tie ® Tension anchor HD340M



Simpson Strong-Tie ® Angle connector AKR135L Angle connector AKR135



Simpson Strong-Tie ® Angle connector AE116

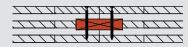


Simpson Strong-Tie ® Angle connector ABR9015

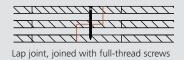
### Joining cross-laminated timber elements together (detail solutions)

Element joints (wall or ceiling)

		V	
	5	$\leq$	
Butt board joined	l w	ith	nails / clamps



Butt joint, joined using external tongue with full-thread screws





Butt floor joint, joined with full-thread screws at 45°

Because of the limited production dimensions, panel joints are often provided parallel to the stress direction. These are either part of the design or – with diaphragm action – produced according to the structural requirements and implemented with milled-in fishplates or external tongues, rebates or butt joints.

**Corner joints CLT walls** Joints with full-thread screws

T joints CLT walls



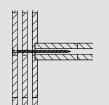
Inset joint, full-thread screws

diagonal from inside

Inset wall joint

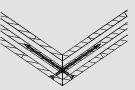


Right-angle butt joint



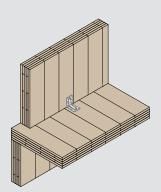
Inset joint, full-thread screws

perpendicular from outside

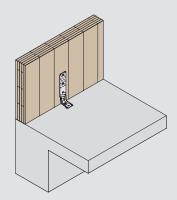


Angled butt joint

Butt joint, inset angles and annular ring nails / screws



Transmission of tensile, transverse and thrust forces with angle connectors (+ annular ring nails/screws), e.g. Simpson Strong-Tie<sup>®</sup> ABR90 / 105. These also serve as assembly aid (stop). Joining the wall with the floor beneath is done with full or partial-thread screws.



Transmission of tensile forces by diaphragm action to the wall ends with tension ties, e.g. Simpson Strong-Tie<sup>®</sup> angle connector AKR. Transmission of thrust forces from horizontal loads (wind) continuous with angles, e.g. ABR90/105/9015 or AE116.



Picture: © Getzner Werkstoffe GmbH

Acoustic protection angle ABA1105 from Simpson Strong-Tie<sup>®</sup>/ Getzner connects construction components without increasing sound transmission.

# **Dimensioning rules for fasteners**

The following summarises the dimensioning rules for fasteners in CLT components in accordance with ETA 11/0189, Appendix 5, to be understood as complementary to EN 1995-1-1.

Information about fasteners in the plane sides is valid only for outer layers made of softwood. Fasteners in the narrow sides of wood panels are not permitted.

### Sizing of fasteners in plane sides of CLT

(Surfaces of construction component II to the panel plane)

Loading	$\perp$ to the	pin axis	II to the pin axis					
Fastener	Shear strength	Conditions	Pull-out resistance	Conditions				
Nails	Hole strength of solid wood taking	$d \ge 4 mm$ $d \ge 6 mm$	$\begin{split} R_{ax,k} &= 14  \cdot  d^{ \varrho \varepsilon}  \cdot  I_{ef} \left[ N \right] \\ profiled nails with d,  I_{ef} \left[ mm \right] \end{split}$	$d \ge 4 mm$ $n \ge 2each join$ $l_{el} \ge 8d$				
self-tapping screws (full-thread screws)	account of molded density of the layers and the angle between stress and fibre orientation of outer layer	d≥6 mm	$\begin{split} R_{ax_ik} &= \sum_{i=1}^n f_{ax_i,k} \cdot I_{ef,i} \cdot d \ [N] \\ f_{ax_i,k} &= char. pullout parameter of layer i, \\ dep. on \rho_{k,i} and angle \alpha_i betw. screw axis & fibre direction of layer i \\ I_{ef,i} &= penetration depth of thread in layer i \\ n &= no. of penetrated layers \end{split}$	$\label{eq:left} \begin{array}{l} d \geq 6 \mbox{ mm} \\ I_{ef,i} \geq 4d \\ \\ \mbox{Thread lengths } I_{ef} \mbox{ applicable if:} \\ \alpha \geq 30^{\circ} \end{array}$				
Dowel pins, fit bolts								
Dowels, see ETA Appendix 5 (1.2)								
General		rs: n <sub>ef</sub> = n for outer layers n <sub>ef</sub> as in EN 1995-1-1 (8.3.1.1)						
				Table 3				

### Sizing of fasteners in narrow sides of CLT

(Surfaces  $\perp$  to the plane sides of the component)

Loading	$\perp$ to the	pin axis	II to the pin axis				
Fastener	Shear strength	Conditions	Pull-out resistance	Conditions			
self-tapping screws (full-thread screws)	$f_{h,k} = 20 \cdot d^{-0.5}$ [N/mm <sup>2</sup> ]	d≥8 mm	$\begin{split} R_{ac,k} = & \sum_{i=1}^{n} f_{ac,i,k} \cdot I_{ef,i} \cdot d \ [N] \\ \text{see table 1 (fastener in plane sides)} \end{split}$	$d \ge 8 \text{ mm}$ others: see table 1 (fastener in plane sides)			
General	Effective no. of fasten n <sub>ef</sub> to EN 1995-1-1 88						
Lateral stress protection against splitting under stress⊥ to CLT plane	h h <sub>e</sub> → Wall Strengthening with full-thread screws	$h_e/h < 0.7 \rightarrow$ lateral stress protection with full-thread screws rqd. $h_e$ = distance of furthest fastener from loaded edge h = thickness of CLT component					

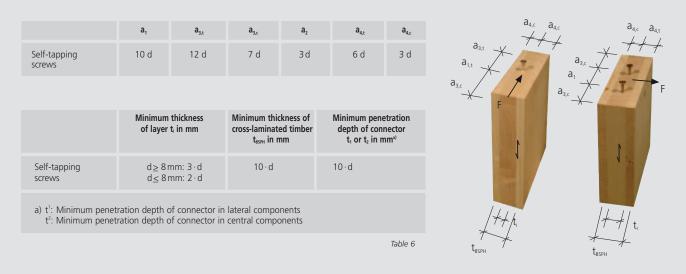
Table 4



Nails $(3+3\cos\alpha)d$ $(7+3\cos\alpha)d$ $6d$ $3d$ $(3+4\sin\alpha)d$ $3d$ Self-tapping screws $4d$ $6d$ $6d$ $2,5d$ $6d$ $2,5d$ $2,5d$ Dowels $(3+2\cos\alpha)d$ $5d$ $max \{ \frac{4d}{3d} \sin \alpha \}$ $3d$ $3d$ $3d$ $3d$ Bolts $max \{ \frac{(3+2\cos\alpha)d}{4d}$ $5d$ $4d$ $4d$ $3d$ $3d$ $3d$	Self-tapping screws4d6d6d2,5d6d2,5dDowels $(3+2\cos\alpha)d$ 5d $max \left\{ \frac{4d}{3d} \sin \alpha \right\}$ 3d3d3dBolts $max \left\{ \frac{(3+2\cos\alpha)d}{4d} \right\}$ 5d4d4d3d3d		a <sub>1</sub>	а <sub>з,t</sub>	a <sub>3,c</sub>	a <sub>2</sub>	a <sub>4,t</sub>	a <sub>4,c</sub>
screwsScre	screwsScre	Nails	(3+3 cos α) d	(7+3 cos α) d	6 d	3 d	(3+4 sin α) d	3d
Bolts $\max \begin{cases} (3+2\cos\alpha)d & 5d & 4d & 4d & 3d & 3d \\ 4d & & \end{cases}$	Bolts $\max \begin{cases} (3+2\cos\alpha)d \\ 4d \end{cases} 5d 4d 4d 3d 3d 3d Table 5$		4 d	6 d	6 d	2,5 d	6 d	2,5 d
	Table 5	Dowels	(3+2 cos α) d	5 d	$\max \left\{ \begin{matrix} 4d \cdot \sin \alpha \\ 3d \end{matrix} \right.$	3 d	3 d	3 d
Table 5		Bolts	$\max \begin{cases} (3+2\cos\alpha)  d \\ 4d \end{cases}$	5 d	4 d	4 d	3 d	3 d
	$+\frac{a_{3,t}}{t}$							Table 5
$ \alpha$ $F$ $\alpha$ $\alpha$ $\beta$ $\alpha$ $\beta$ $\alpha$ $\beta$ $\alpha$ $\beta$ $\alpha$ $\beta$ $\alpha$ $\beta$ $\beta$ $\alpha$ $\beta$				F				

### Minimum separation of fasteners in plane sides of cross-laminated timber components

### Minimum separation of fasteners in narrow sides of cross-laminated timber components



Tables 5 & 6 and graphics are from the European Technical Approval for cross-laminated timber (ETA 11/0189, p. 18-21). By kind permission of the German Institute for Building Technology (DIBt, Deutsches Institut für Bautechnik). The full document is available for download from our website (www.derix.de).



# Roof Draft design

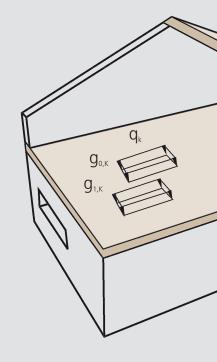
The tables provide support in planning your projects - they are not a substitute for structural calculations.

[kN/m²]		[kN/m²] Snow	Span length single-span beam L [m]																							
Constant applied load g <sub>1,k</sub> <sup>2)</sup>	SLZ <sup>3)</sup>	load S <sub>k</sub>	3.0	3.5	4.0	4.5	5.0	5.5	6.0	7.0																
	1	0,65			L-80/3s	L-90/3s	L-100/3s	L-110/3s	L-120/3s																	
0.25	2	0,85	L-60/3s			L-00/33	L-J0/J3	L-100/35		L-130/5s	L-160/5s															
	3	1,10						L-120/3s		L-100/33																
	1	0,65					L-110/3s	2 120/33																		
0.50	2	0,85		L-80/3s	L-90/3s	L-100/3s			L-140/5s																	
	3	1,10							1 120/Ec		L-170/5s															
	1	0,65																					L-120/3s	L-130/5s		
0.75	2	0,85	L-80/3s																							
	3	1,10			L-100/3s	L-110/3s		L-140/33	L-160/5s	L 100/33																
	1	0,65		L-90/3s	L-100/35			L-160/5s	L-100/33	LL-190/7s																
1.50	2	0,85		2 50/33	L-110/3s	L-120/3s	L-140/5s		1 170/Ec	LL 130/73																
	3	1,10		L-100/3s	2 1 10/00				L-170/5s	LL-210/7s																
										Table 7																

Application limits for cross-laminated timber components based on flexure<sup>1)</sup> (F)

[kN/m²]	[kN/m²]	Span length double-span beam L [m]																					
Constant applied load g <sub>1,k</sub> <sup>2)</sup>	SLZ <sup>3)</sup>	Snow load S <sub>k</sub>	3.0	3.5	4.0	4.5	5.0	5.5	6.0	7.0													
	1	0,65		L-60/3	L-60/3s		1.00/2-	1.00/2-		L-110/3s													
0.25	2	0,85					L-80/3s	L-90/3s	1 100/2*	L-120/3s													
	3	1,10	L-60										L-90/3s	L-100/3s	L-100/3s	L-130/5s							
	1	0,65			L-60/3s		1.00/2*	L-80/3s	L-90/3s		L-120/3s												
0.50	2	0,85		3s L-80/3s			L-80/3s				L-130/5s												
	3	1,10	L-60/3s			1.00/2c		L-90/3s	L-100/3s	L-110/3s	L-140/5s												
	1	0,65																L-00/35		L-90/35	L-100/33	L-110/33	L-130/5s
0.75	2	0,85										L-140/5s											
	3	1,10						1 120/2-	2110/33														
	1	0,65	L-80/3			L-90/3s	L-100/3s	L-110/3s	L-120/3s	L-150/5s													
1.50	2	0,85										1.120/5-	1.100/5-										
	3	1,10	L-80/3s		L-90/3s	L-100/3s	L-110/3s	L-120/3s	L-130/5s	L-160/5s													
										Table 8													

[kN/m²]		[kN/m²]			Span	ength trip	le-span bea	am L[m]																	
Constant applied load g <sub>1,k</sub> <sup>2)</sup>	SLZ <sup>3)</sup>	Snow load S <sub>k</sub>	3.0	3.5	4.0	4.5	5.0	5.5	6.0	7.0															
	1	0,65		1.00/2:			L-80/3s	L-90/3s	L-100/3s	L-120/3s															
0.25	.25 2 0	0,85		L-60/3s						L-130/5s															
	3	1,10		L-80/3s		L-80/3s	L-90/3s	L-100/3s	L-110/3s	L-140/5s															
	1	0,65	L-60/3s	L-60/3s			2 50,55	2 100/33	2 110/33	L-130/5s															
0.50	2	0,85		L-60/3s	L-60/3s	L-60/3s	L-60/3s	L-60/3s	L-60/3s	L-60/3s		L-80/3s													
	3	1,10		L-80/3s							L-110/3s		1 1 4 0 / 5 -												
	1	0,65																						L-90/3s	L-100/3s
0.75	2	0,85				L-20/22	L-100/35	L-110/3s	L-120/35																
	3	1,10						L-110/35																	
	1	0,65						L-120/3s		L-160/5s															
1.50	2	0,85	L-80/3s		L-90/3s	L-100/3s	L-110/3s	L-120/35	L-140/5s	L 100/33															
	3	1,10							L-130/5s																
										Table 9															



 $g_{\mbox{\tiny 0,k}}\mbox{=}$  constant load from component's own weight  $g_{_{1,k}}$  = constant applied load (ceiling or roof superstructure)  $q_k$  = imposed load s<sub>i</sub>=snow load on the roof  $w_{\scriptscriptstyle e}{=}\,wind$  pressure on roof surface

Identification of elements for fire resistance as in EN 1995-1-2 (1-sided burning, below;  $\beta_0 = 0.65$  mm/min)

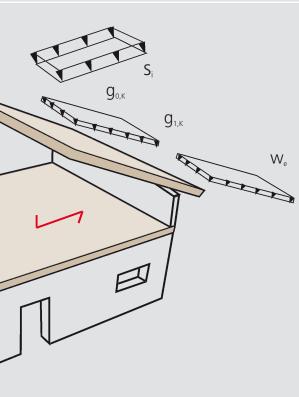
L-60/3s	R0 (F0)
L-100/3s	R30 (F30)
L-130/5s	R90 (F90)

<sup>1)</sup> Deformation factor as BS EN 1995-1-1 for service class 1:  $k_{def} = 0.8$ ; limit values of deformation as in BS EN 1995-1-1/NA;  $w_{inst} = L/300$ ;  $w_{fin} = L/150$ ;  $w_{net,fin} = L/25$ <sup>2)</sup> Additional load  $g_{1,k}$ ; the elements' own weight is already allowed for in the results with  $\rho = 450 \text{ kg/m}^3$ . <sup>3)</sup> The table uses the stated basic amounts for  $s_k$ . For higher values separate calculations are required.

# Ceiling (single span beam) **Draft design**

The tables can help to plan your projects – but they do not replace structural calculations.

www.x-lam.de/dimensioning



Application limits for cross-laminated timber components based on flexure<sup>1)</sup> (F)

[kN/m²] Constant	[kN/m²] Live load	Span length single-span beam L [m]										
applied load g <sub>1,k</sub> 2)	<b>q</b> <sub>k</sub> <sup>3)</sup>	3,0	3,5	4,0	4,5	5,0	5,5	6,0	7,0			
	1.5 2.0	L-80/3s	L-90/3s	L-100/3s	L-110/3s L-120/3s	L-130/5s L-140/5s	L-140/5s L-150/5s	L-160/5s	LL-190/7s			
0.5	3.0	L-90/3s	L-100/3s	L-110/3s	L-130/5s	L-150/5s	L-160/5s	L-180/5s	LL-210/7s			
4	4.0	L-90/35	1 440/2	L-120/3s	L-140/5s	L-160/5s	L-180/5s	LL-190/7s	LL-230/7s			
	5.0	L-100/3s	L-110/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s	LL-210/7s	LL-240/7s			
2.0 1.0 3.0 4.0	1.5	L-80/3s	L-90/3s	L-110/3s	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s			
	2.0	L-00/35	L-100/3s	L-110/35	L-130/5s	L-140/33	L-100/33	L-180/5s	LL-210/7s			
	3.0	L-90/3s	L 100/33	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s	LL-230/7s			
	4.0	L-100/3s	L-110/3s	L-130/5s	L-150/5s		LL-190/7s		LL-240/7s			
	5.0	L 100/33	L-120/3s	L-140/5s	L-160/5s	L-180/5s	LL 150/75	LL-210/7s	LL-240/73			
	1.5	L-90/3s	-90/3s L-100/3s	L-110/3s	L-130/5s	L-150/5s	L-160/5s	L-180/5s	LL-210/7s			
	2.0			L-120/3s	L-160/5s	L-170/5s	LL-190/7s	LL-230/7s				
1.5	3.0		L-110/3s	L-130/5s			L-180/5s					
	4.0	L-100/3s	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s	LL-210/7s	LL-240/7s			
	5.0					L-180/5s		2210/75	LL-260/7s			
	1.5	L-90/3s	L-100/3s	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s	L-220/7s			
	2.0	2 5 6, 5 5	L-110/3s	L-130/5s			L-180/5s		LL-230/7s			
2.0	3.0 4.0	L-100/3s	L-120/3s	L-140/5s	L-160/5s	L-170/5s L-180/5s	LL-190/7s	LL-210/7s	LL-240/7s			
	5.0	L-110/3s	L-130/5s	L-150/5s	L-170/5s	L-190/7s	LL-210/7s	LL-230/7s	LL-260/7s			

Table 10

Application limits for cross-laminated timber components based on vibration<sup>4)</sup> (S)

[kN/m²] Constant	[kN/m²] Live load		Span length single-span beam L [m]														
applied load g <sub>1,k</sub> <sup>2)</sup>	<b>q</b> <sub>k</sub> <sup>3)</sup>	3,	3,0 3		,5 4,0		4,5		5,0		5,5		6,0		7,0		
		S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S <u>(</u> >6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)
	1.5 2.0		L-80/3s		L-90/3s		L-100/3s		L-110/3s L-120/3s		L-140/5s		L-160/5s		L-190/7s		
0.5	3.0		L-90/3s		L-100/3s		L-110/3s		L-130/5s		L-150/5s	Ц	1.100/5-		2 100/75		LL-240/7s
	4.0 5.0		L-100/3s		L-110/3s		L-120/3s L-140/5s		L-140/5s L-160/5s		L-160/5s L-170/5s		L-180/5s LL-190/7s				
	1.5 2.0		L-80/3s		L-90/3s		L-140/3s		L-130/5s				L-180/5s				
1.0	3.0		L-90/3s		L-100/3s	L-120/5s		L-140/5s		L-160/5s		2 100/00		LL-210/7s		LL-260/7s	
	4.0		L-100/3s	L-130/5s	L-110/3s		L-130/5s	0/5s L-170/5s 0/3s	L-150/5s	LL-190/7s		11 210/74	s 1.21		220/7c	L-260/7s	
	5.0 1.5	L-110/3s	L-90/3s		L-120/3s	L-150/5s	L-140/5s L-120/3s		L-160/5s			LL-210/7s	/s LL-190/7s	L-220/7s	S		
	2.0		L-90/22						L-150/5s		L-180/5s						
1.5	3.0				L-110/3s		L-130/5s								LL-230/7s		
	4.0 5.0		L-100/3s		L-120/3s												L-300/9s
	1.5 2.0		L-90/3s		L-110/3s		L-140/5s		L-160/5s								
2.0	3.0 4.0		L-100/3s		L-120/3s						LL-190/7s		LL-210/7s		LL-240/7s		
	5.0		L-110/3s		L-130/5s		L-150/5s		L-170/5s					LL-230/7s			
																	Table 11

<sup>10</sup> Deformation factor as in BS EN 1995-1-1 for service class 1: k<sub>def</sub> = 0.8; limit values of deformation as in BS EN 1995-1-1/NA; w<sub>inst</sub> = L/300; w<sub>lin</sub> = L/150; w<sub>net,fin</sub> = L/250

<sup>2)</sup> Additional load  $g_{1,k}$  excluding component weight  $g_{0,k}$  (this is already allowed for in the results with  $\rho = 450 \text{ kg/m}^3$ .)

<sup>3)</sup> Live load categories as in BS EN 1991-1-1/NA 1DE: A (living areas) or B (office areas)

<sup>4</sup> Basis for calculation, general: damping 2.5%, disturbing vibrations in the adjacent span, no account of stiffness of screed Hamm/Richter: assessment 1.5-2.5; ceilings in one use unit, e.g. ceilings in single-family houses, existing ceilings or by agreement with the client; natural frequency  $f \ge 6$  Hz; Stiffness w(2kN)  $\le 1.0$  mm with  $b_{eff} = 1$  m; design requirements (bare floor, fill, screed) to be allowed for. BS EN 1995-1-1/NA: natural frequency  $f \ge 8$  Hz; stiffness w(1 kN)  $\le 2.0$  mm (all sections meet the normal requirements); vibration velocity v

# Ceiling (double span beam) **Draft design**

The tables can help to plan your projects – but they do not replace structural calculations.

[kN/m²] Constant applied	[kN/m²] Live load	Span length double-span beam L [m]											
load g <sub>1,k</sub> <sup>2)</sup>	q <sub>k</sub> <sup>3)</sup>	3.0	3.5	4.0	4.5	5.0	5.5	6.0	7.0				
	1.5	L-60/3s	L-80/3s	L-80/3s	L-90/3s	L-100/3s	L-110/3s	L-120/3s	L-150/5s				
	2.0		2 00,00	L-90/3s	L-100/3s	L-110/3s	L-120/3s	L-140/5s	L-160/5s				
0.5	3.0	L-80/3s	L-90/3s	L-100/3s	L-110/3s	L-120/3s	L-140/5s	L-160/5s	L-180/5s				
	40		L-90/35	L-100/33	L-120/3s	L-140/5s	L-160/5s	L-100/35	LL-190/7s				
	5.0	L-90/3s	L-100/3s	L-110/3s	L-130/5s	L-140/33	L-100/33	L-180/5s	LL-210/7s				
1.0	1.5		L-80/3s	L-90/3s	L-100/3s	L-110/3s	L-120/3s	L-130/5s	L-160/5s				
	2.0	L-80/3s	2 00,00	L-J0/J3	L-100/33	L-120/3s	L-130/5s	L-140/5s	L-170/5s				
	3.0		L-90/3s	L-100/3s	L-110/3s	L-130/5s	L-140/5s	L-160/5s	LL-190/7s				
	4.0		L-100/3s	L-110/3s	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-150/75				
	5.0	L-90/3s	L-100/33	L-120/3s	L-140/5s	L-150/5s	2 100/33	L-180/5s	LL-210/7s				
	1.5	L-80/3s	L-80/3s	L-90/3s	L-100/3s	L-130/5s	L-130/5s	L-140/5s	L-170/5s				
	2.0		L 00/33	L-100/3s	L-110/3s	L-130/35	L-140/5s	L-160/5s	L-180/5s				
1.5	3.0	L 00/33	L-90/3s	L-100/35	L-120/3s	L-140/5s	L-150/5s	L-100/33	LL-190/7s				
	4.0		L-100/3s	L-100/3s	L-130/5s	L 140/33	L-160/5s	L-180/5s	LL-210/7s				
	5.0	L-90/3s	L-100/33	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s	LL-230/7s				
	1.5		L-80/3s	L-100/3s	L-110/3s	L-130/5s	L-140/5s	L-150/5s	L-180/5s				
	2.0	L-80/3s	L-90/3s	2 100/00	L-110/3s	2-120/25	L-140/JS	L-160/5s	L-180/55				
2.0	3.0		L-100/3s	L-110/3s	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s				
	4.0		L-100/35	L-120/3s	L-130/5s	L-150/5s	L-100/35	L-180/5s	LL-210/7s				
	5.0	L-90/3s	L-110/3s	L-120/35	L-140/5s	L-160/5s	L-170/5s	LL-190/7s	L-220/7s				

Application limits for cross-laminated timber components based on flexure<sup>1)</sup> (F)

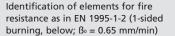


Table 13



Table 12

Application limits for cross-laminated timber components based on vibration<sup>4)</sup> (S)

[kN/m²] Constant	[kN/m²] Live load		Span length double-span beam L [m]														
applied load g <sub>1,k</sub> <sup>2)</sup>	<b>q</b> <sub>k</sub> <sup>3)</sup>	3.	3.0 3.		.5	i 4.0		4.5		5.0		5.5		6.0		7.0	
		S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)
	1.5		L-60/3s		L-80/3s		L-90/3s										
	2.0				L-80/35		L-90/35		L-110/3s	L-140/5s				L-190/7s			
0.5	3.0		L-80/3s		L-90/3s		L-100/3s					L-160/5s				LL-240/7s	
	4.0								L-120/3s								
	5.0		L-90/3s		L-100/3s												
1.0	1.5				1 00/0	L-140/5s	1 110/2-		L-130/5s			L-180					
	2.0		L-80/3s		L-90/3s		L-110/3s				L 100/Es		L-180/5s		11 240/7		11 200/7*
1.0	3.0 4.0										L-160/5s		L 100/33		LL-210/7s		LL-260/7s
	5.0	L-100/3s	L-90/3s	1 120/24				L-160/5s	L-140/5s	L-170/5s	LL-190/	LL-190/7s		L-220/7s		L-240/7s	
	1.5	L-100/35	2 50/55	L-120/3s					2 1 10/33	L-1/0/55				L-220/73		L-240/75	
	2.0				L-100/3s				L-150/5s		L-180/5s						
1.5	3.0		L-80/3s				L-120/3s						LL-190/7s		LL-230/7s		
	4.0																
	5.0		L-90/3s														1 200/06
	1.5																L-300/9s
	2.0	L	1.00/2-	L-110/3s	1 110/2-		L 140/E-		L 160/E-								
2.0	3.0		L-90/3s		L-110/35		L-140/5s		L-160/5s		LL-190/7s	LL-1	LL-210/7s		LL-240/7s		
	4.0																
	5.0																

<sup>10</sup> Deformation factor as in BS EN 1995-1-1 for service class 1: k<sub>def</sub> = 0.8; limit values of deformation as in BS EN 1995-1-1/NA; w<sub>inst</sub> = L/300; w<sub>fin</sub> = L/150; w<sub>net,fin</sub> = L/250

<sup>2)</sup> Additional load  $g_{1,k}$  excluding component weight  $g_{0,k}$  (this is already allowed for in the results with  $\rho = 450 \text{ kg/m}^3$ .)

<sup>39</sup> Live load categories as in BS EN 1991-1-1/NA 1DE: A (living areas) or B (office areas)

<sup>4</sup> Basis for calculation, general: damping 2.5%, disturbing vibrations in the adjacent span, no account of stiffness of screed

Hamm/Richter: assessment 1.5-2.5; ceilings in one use unit, e.g. ceilings in single-family houses, existing ceilings or by agreement with the client; natural frequency  $f \ge 6$  Hz; Stiffness w(2kN)  $\le 1.0$  mm with  $b_{eff} = 1$  m; design requirements (bare floor, fill, screed) to be allowed for. BS EN 1995-1-1/NA: natural frequency  $f \ge 8$  Hz; stiffness w(1 kN)  $\le 2.0$  mm (all sections meet the normal requirements); vibration velocity v

<b>Application example for draft-design tables</b> Ceiling structure:			
Tiles (8 mm):	0.22 kN/m²/cm x 0.8 cm	=	0.18 kN/m²
Cement screed (6 cm):	0.22 kN/m²/cm x 6.0 cm	=	1.32 kN/m <sup>2</sup>
Impact sound insulation (EPS) (6 cm):	0.35 kN/m³ x 0.06 m	=	0.02 kN/m <sup>2</sup>
Gypsum fibreboard 2x (impact sound):	0.09 kN/m²/cm x 2 x 1.25 cm	=	0.23 kN/m <sup>2</sup>
X-LAM ceiling component: The own-weight is already allowed for in th	e results.		
Battens (24/48, e = 50 cm)	6.00 kN/m³ x 0.024 m x 0.048 m /0.50 m	=	0.01 kN/m²
Gypsum plasterboard (2x):	0.09 kN/m²/cm x 2 x 1.25 cm	=	0.23 kN/m <sup>2</sup>
	constant applied load $g_{_{1,k}}$	=	1.99 kN/m²
Live load category B1	Traffic load q <sub>k</sub>	=	2.00 kN/m <sup>2</sup>
(office area)	Added for partition wall $\Delta q_{_k}$	=	0.80 kN/m²
	$\Sigma$ variable load $q_{\scriptscriptstyle k}$	=	2.80 kN/m <sup>2</sup>
Input values for the reading: $g_{1,k} = 2.00 \text{ kN/m}^2$ ; $q_k = 3.00 \text{ kN/m}^2$ ; Span length L = 4.50 m (double-span b	eam)		»required cross-laminated timber L-120/3s deflection analysis; L-160/5s vibration analysis



# Ceiling (triple span beam) **Draft design**

The tables can help to plan your projects – but they do not replace structural calculations.

[kN/m²] Constant	[kN/m²] Live load	Span length triple-span beam L [m]												
applied load g <sub>1,k</sub> 2)	<b>q</b> <sub>k</sub> <sup>3)</sup>	3.0	3.5	4.0	4.5	5.0	5.5	6.0	7.0					
	1.5	L-80/3s	L-80/3s	L-90/3s	L-100/3s	L-110/3s	L-120/3s	L-130/5s	L-160/5s					
	2.0		L-00/35	2 50,55	L-100/33	L-110/33	L-130/5s	L-140/5s	L-170/5s					
0.5	3.0	2 00/33	L-90/3s	L-100/3s	L-110/3s	L-130/5s	L-140/5s	L-160/5s	LL-190/7s					
	4.0		L-100/3s	L-110/3s	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-1 <i>J0/1</i> 3					
	5.0	L-90/3s	L-100/35	L-120/3s	L-140/5s	L-160/5s	L-100/33	L-180/5s	LL-210/7s					
	1.5	L-80/3s	1.00/2*	L-90/3s	L-100/3s	L-110/3s	L-130/5s	L-140/5s	L-170/5s					
1.0	2.0		L-80/3s	L-100/3s	L-110/3s	L-120/3s	L-140/5s	1.460/5	L-180/5s					
	3.0		L-90/3s	L-100/35	L-120/3s	1.1.10/5-	L-160/5s	L-160/5s	LL-190/7s					
	4.0	L-90/3s	L-100/3s	L-110/3s	L-130/5s	L-140/5s	L-100/55	L-180/5s	LL-210/7s					
	5.0		L-100/35	L-120/3s	L-140/5s	L-160/5s	L-170/5s	LL-190/7s						
	1.5	L-80/3s	L-80/3s	L-100/3s	L-110/3s	L-120/3s	L-140/5s	L-160/5s	L-180/5s					
	2.0		L-90/3s	L-100/33	L-110/35	L-130/5s	L-140/55	L-100/35	LL-190/7s					
1.5	3.0		L-100/3s	L-110/3s	L-120/3s	L-140/5s	L 100/Es	L-170/5s	LL-190/75					
	4.0	L-90/3s	L-100/55	L-120/3s	L-140/5s	L-160/5s	L-160/5s	L-180/5s	LL-230/7s					
	5.0	L-90/35	L-110/3s	L-130/5s	L-140/35	L-100/33	L-180/5s	LL-190/7s						
	1.5	L-80/3s	L-90/3s	L-100/3s	L-110/3s	L-130/5s	L-140/5s	L-160/5s	LL-190/7s					
	2.0	L-00/35	L 30/33	L-100/33	L-120/3s	L-140/5s	L-160/5s	2 100/00	22 100/15					
2.0	3.0	L-90/3c		L-110/3s	L-130/5s	140/05	E-100/35	L-180/5s	LL-210/7s					
2.0	4.0	L-90/3s		L-120/3s	L 140/E-	L 160/Ec	L-170/5s	11 100/7-	22 210/75					
	5.0	L-100/3s		L-130/5s	L-140/5s	L-160/5s	L-180/5s	LL-190/7s	LL-240/7s					
									Table 1					

Application limits for cross-laminated timber components based on flexure<sup>1)</sup> (F)

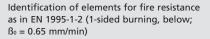


Table 15

L-60/3s R0 (F0) L-100/3s R30 (F30) L-130/5s R90 (F90)

Application limits for cross-laminated timber components based on vibration<sup>4)</sup> (S)

[kN/m²]	[kN/m²]							Spa	an length tri	iple-span be	am L [m]						
Constant applied	Live load $q_k^{3)}$	3.0		3.5		4.0		4.5		5.0		5.5		6.0		7.0	
applied load g <sub>1,k</sub> <sup>2)</sup>		S (≥6Hz)	S <u>(</u> ≥8Hz)	S ( <u>&gt;</u> 6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)	S (≥6Hz)	S (≥8Hz)
	1.5 2.0	L-81	L-80/3s	1-80/35	L-80/3s		L-90/3s		L-110/3s		L-140/5s						LL-240/7s
0.5	3.0 4.0		2 00/00		L-90/3s		L-100/3s L-110/3s		L-120/3s		L 140/33		L-160/5s		L-190/7s		
	5.0		L-90/3s	L-90/3s		L-120/3s		L-140/5s		L-160/5s							
1.0	1.5 2.0 3.0		L-80/3s		L-110	L-110/3s		L-130/5s		L-160/5s		L-180/5s		LL-210/7s	7s LL-230/7s	LL-260/7s	
	4.0 5.0	L-100/3s	L-90/3s		L-14	L-140/5s	L-120/3s		L-140/5s	L-170/5s		LL-190/7s	LL-19	LL-190/7s			
1.5	1.5 2.0 3.0		L-80/3s		L-100/3s				L-150/5s		L-180/5s		LL-190/7s		LL-230/7s	LL·	LL-300/9s
	4.0 5.0						L-130/5s										
2.0	1.5 2.0 3.0 4.0		L-90/3s		L-110/3s		L-140/5s		L-160/5s		LL-190/7s		LL-210/7s		LL-240/7s	LL-240/7s	LL-300/9s
	5.0		L-100/3s														

<sup>1)</sup> Deformation factor as in BS EN 1995-1-1 for service class 1:  $k_{def} = 0.8$ ; limit values of deformation as in BS EN 1995-1-1/NA;  $w_{inst} = L/300$ ;  $w_{fin} = L/150$ ;  $w_{net,fin} = L/250$ 

<sup>2)</sup> Additional load  $g_{1,k}$  excluding component weight  $g_{0,k}$  (this is already allowed for in the results with  $\rho = 450$  kg/m<sup>3</sup>.)

<sup>3)</sup> Live load categories as in BS EN 1991-1-1/NA 1DE: A (living areas) or B (office areas)

<sup>a</sup> Basis for calculation, general: damping 2.5%, disturbing vibrations in the adjacent span, no account of stiffness of screed Hamm/Richter: assessment 1.5-2.5; ceilings in one use unit, e.g. ceilings in single-family houses, existing ceilings or by agreement with the client; natural frequency  $f \ge 6$  Hz; Stiffness w(2kN)  $\le 1.0$  mm with  $b_{eff} = 1$  m; design requirements (bare floor, fill, screed) to be allowed for. BS EN 1995-1-1/NA: natural frequency  $f \ge 8$  Hz; stiffness w(1 kN)  $\le 2.0$  mm (all sections meet the normal requirements); vibration velocity v

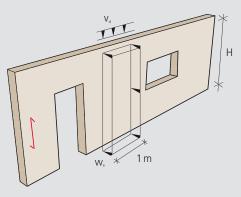
# Wall **Draft design**

The tables can help to plan your projects – but they do not replace structural calculations.

### Draft-design table for wall components

Application limits for cross-laminated timber components based on load-bearing capacity (interaction M+N)

Fire protection <sup>1)</sup>	Application <sup>2)</sup>	Height H	Vertical load $v_{\scriptscriptstyle d}{}^{\scriptscriptstyle 3}$ at wall head [kN/m]						
		[m]	40	60	80				
RO	Exterior wall	1.5 2.8	X-60/3s	X-60/3s	X-60/3s				
(FO)	Exterior wait	3.5	V-00/33		X-70/3s				
		4.5		X-70/3s	X-80/3s				
R30 (F30) 1-sided	Interior/ exterior wall	1.5 2.8 3.5 4.5		X-100/5s					



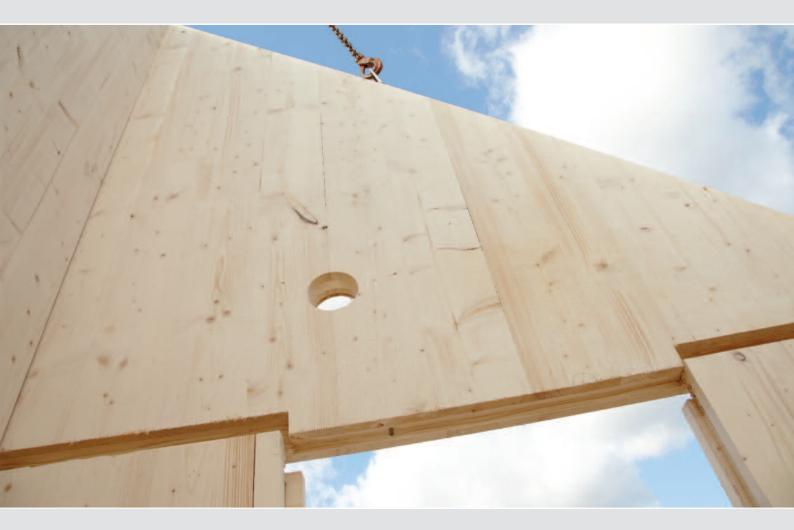
 $v_d$  = design value of vertical load [kN/m]  $w_{\scriptscriptstyle e}\!=\!wind$  pressure on exterior wall in [kN/m²]

 $^{\scriptscriptstyle 1)}$  Fire rating to BS EN 1995-1-2:  $k_{mod,fi}$  = 1.0 and  $\gamma_{M,fi}$  = 1.0

<sup>10</sup> Fire rating to BS EN 1995-1-2:  $k_{mod,fi} = 1.0$  and  $\gamma_{M,fi} = 1.0$ <sup>21</sup> For wall designs up to wind load zone 2 inland, wind loadings are not decisive. Exterior pressure coefficient  $c_{pe} = 0.8$  (range D); resulting  $w_{ind}$  pressure we = 0.8\*q<sup>31</sup> The normal force component from the element's own weight with  $p = 450 \text{ kg/m}^3$  is already included in the results. For the fire rating the corresponding design value  $v_{d,fi}$  should be used. Basis for calculation: Equivalent member method with buckling length = height H; 1 m wide wall strip; NKL 1; System coefficient  $k_1 = 1.0$ ; Design location in wall centre (H/2)



Table 16



Our experts are the perfect consultants for any kind of project to be realised: complex designs, international projects or efficient planning. Please don't hesitate to benefit from our expertise regarding all kinds of laminated timber constructions.









W. u. J. Derix GmbH & Co. Laminated Timber Dam 63 · 41372 Niederkrüchten · Germany Tel +49/2163/89880 · Fax +49/2163/898887 info@derix.de · www.derix.de



Poppensieker & Derix GmbH & Co. KG Laminated Timber Industriestraße 24 · 49492 Westerkappeln · Germany Tel +49/5456/93 03 0 · Fax +49/5456/93 03 30 info@poppensieker-derix.de · www.poppensieker-derix.de

